

## Four channel Wigner-Smith matrix formalism applied to the scattering by a fluid layer embedded in semi infinite solids

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### Abstract :

The acoustic scattering by a fluid slab between two semi infinite solid media is revisited from the point of view of a four channel resonant scattering formalism. For a plane and monochromatic longitudinal ( $P=L$ ) or transversal ( $P=T$ ) wave incident from each solid, the reflection coefficients  $r^{PQ}$  and transmission coefficients  $t^{PQ}$  by the fluid layer ( $Q=L$ , or  $T$  represents the polarization of the scattered waves) are the components of a  $4 \times 4$  symmetric, unitary scattering matrix  $\mathbf{S}$  ( $\mathbf{S}^\dagger \mathbf{S} = \mathbf{S} \mathbf{S}^\dagger = \mathbf{I}$ ). In the particular case of identical solids, it is shown that  $\mathbf{S}$  has to be written as the product of 2 unitary scattering matrices:  $\mathbf{S}^{(b)}$  - corresponding to the scattering by the vacuumed layer-, and  $\mathbf{S}^{(*)}$  - denoting the pure resonant part of  $\mathbf{S}$ -. The Wigner-Smith matrix  $\mathbf{Q}_{x_i} = -j(\partial_{x_i} \mathbf{S}) \mathbf{S}^\dagger$  is analyzed ( $\partial_{x_i}$  is the partial derivative with respect to a given input parameter  $x_{i=1,...,4} = f, c_L, c_T, c_F$ ), this formalism being the multichannel extension of Phase Gradient Method.

### Résumé :

L'étude de la diffusion acoustique par un slab fluide entre deux solides homogènes est réexaminée dans le cadre du formalisme de la matrice  $\mathbf{S}$  de diffusion résonnante à 4 canaux. Considérant une onde incidente plane monochromatique longitudinale ( $P=L$ ) ou transversale ( $P=T$ ), la matrice de diffusion  $\mathbf{S}$  ( $4 \times 4$ ) symétrique unitaire est élaborée à partir des coefficients de réflexion  $r^{PQ}$  et de transmission coefficients  $t^{PQ}$  par la couche fluide ( $Q=L$ , ou  $T$  représente la polarisation des ondes diffusées). Dans le cas particulier de solides identiques, on montre que  $\mathbf{S}$  s'écrit comme produit de 2 matrices de diffusion unitaires:  $\mathbf{S}^{(b)}$  - matrice de diffusion de la couche vide-, and  $\mathbf{S}^{(*)}$  - contribution purement résonnante de  $\mathbf{S}$ -. Le formalisme de la matrice de Wigner-Smith  $\mathbf{Q}_{x_i} = -j(\partial_{x_i} \mathbf{S}) \mathbf{S}^\dagger$  est alors mis en place ( $\partial_{x_i}$  est la dérivée partielle par rapport à l'un des paramètres d'entrée  $x_{i=1,...,4} = f, c_L, c_T, c_F$ ), afin de généraliser la Méthode des Gradients de Phase à une situation de diffusion multicanal.

### Keywords :

Multichannel Scattering ; Phase Gradient ; Wigner-Smith Matrices

## 1 Construction of the $\mathbf{S}$ matrix

The present work is intended to prepare studies on effective medium approximations of a slab region randomly filled with scatterers in a solid. Let consider the simple problem of the scattering by a fluid layer  $F_2$  (thickness  $d$ , density  $\rho_F$ , phase velocity  $c_F$ ) between two semi infinite solids  $S_1$  and  $S_3$  (density  $\rho_{S,m}$ , longitudinal and transversal phase velocities  $c_{L,m}$  and

$c_{T,m}$ ,  $m=1,3$ ) sketched in FIG. 1. As for a plane and monochromatic incident wave (frequency  $f$ , incidence angle  $\theta_p$ ) from each solid  $S_m$  ( $m=1,3$ ), two elementary polarizations  $P=L$ , or  $T$  ( $L$  for longitudinal,  $T$  for transversal) are available, such a study requires the multichannel framework provided by the scattering matrix  $\mathbf{S}$  formalism.

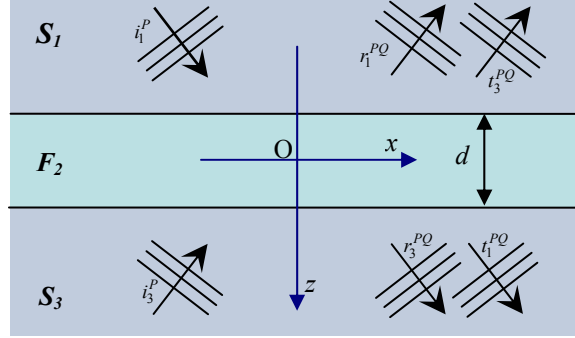


FIG. 1 – Geometrical configuration

Assuming the continuity of the normal and tangential stress components and the normal displacement component at the boundaries  $z = \pm d/2$ , the reflection  $r_m^{PQ}$  and transmission  $t_m^{PQ}$  coefficients of the structure are needed to build the  $\mathbf{S}$  matrix. Their expression are (1)

$$\begin{aligned} r_m^{LL} &= \left[ (C_{A,m}^- + i\tau_m)(C_{S,n}^+ - i\tau_n) + (C_{A,n}^+ + i\tau_n)(C_{S,m}^- - i\tau_m) \right] / D, \\ r_m^{LT} &= -4k_x k_{zL,m} (2k_x^2 - k_{T,m}^2) \left[ T(C_{S,n}^+ - i\tau_n) + C(C_{A,n}^+ + i\tau_n) \right] / D, \quad r_m^{TL} = (k_{zT,m} / k_{zL,m}) r_m^{LT}, \\ r_m^{TT} &= \left[ (C_{A,m}^- - i\tau_m)(C_{S,n}^+ - i\tau_n) + (C_{A,n}^+ + i\tau_n)(C_{S,m}^- + i\tau_m) \right] / D, \\ t_m^{LL} &= (\alpha_m / \alpha_n) \left[ (C_{A,n}^+ + i\tau_n)(C_{S,n}^+ - i\tau_n) - (C_{A,n}^+ + i\tau_n)(C_{S,n}^- - i\tau_n) \right] / D, \\ t_m^{LT} &= 4k_x k_{zL,m} (k_{T,m}^2 / k_{T,n}^2) (2k_x^2 - k_{T,m}^2) \left[ T(C_{S,n}^+ - i\tau_n) - C(C_{A,n}^+ + i\tau_n) \right] / D, \\ t_m^{TL} &= 4k_x k_{zL,m} k_{T,m}^2 / (k_{zL,n} k_{T,n}^2) k_{zT,m} (2k_x^2 - k_{T,m}^2) \left[ T(C_{S,n}^+ - i\tau_n) - C(C_{A,n}^+ + i\tau_n) \right] / D, \\ t_m^{TT} &= -(\alpha_n / \alpha_m) \left[ (C_{A,n}^- - i\tau_n)(C_{S,n}^+ - i\tau_n) - (C_{A,n}^+ + i\tau_n)(C_{S,n}^- + i\tau_n) \right] / D, \end{aligned}$$

where (2)

$$\begin{aligned} D &= (C_{A,m}^+ + i\tau_m)(C_{S,n}^+ - i\tau_n) + (C_{A,n}^+ + i\tau_n)(C_{S,m}^+ - i\tau_m), \\ C_{A,m}^\pm &= R_m^\pm T, \quad C_{S,m}^\pm = R_m^\pm C, \quad \tau_m = (\rho_F / \rho_S)(k_{zL,m} / k_{zF}), \\ R_m^\pm &= 4k_x^2 k_{zL,m} k_{zT,m} \pm (2k_x^2 - k_{T,m}^2)^2, \quad T = C^{-1} = \tan(\pi f k_{zF} d), \\ \alpha_m &= (-i) 2k_{T,m}^2 (k_{zL,m} / k_{zF})(2k_x^2 - k_{T,m}^2). \end{aligned}$$

The indexes  $m=1,3$  and  $n \neq m$  stand for the incidence solid medium and the second solid medium respectively. Denoting by  $\theta_{L,m}$  and  $\theta_{T,m}$  the longitudinal and transversal incidence angles respectively and by  $\theta_F$  the refraction angle in the fluid, the projections of the involved normalized wave vectors ( $k_{L,m} = 1/c_{L,m}$ ,  $k_{T,m} = 1/c_{T,m}$ ,  $k_F = 1/c_F$ ) are  $k_x = \sin \theta_{L,m} / c_{L,m} = \sin \theta_{T,m} / c_{T,m} = \sin \theta_F / c_F$  along the  $x$ -axis,  $k_{zL,m} = \cos \theta_{L,m} / c_{L,m}$ ,  $k_{zT,m} = \cos \theta_{T,m} / c_{T,m}$ , and  $k_{zF} = \cos \theta_F / c_F$  along the  $z$ -axis. In the symmetric case of two identical solid media surrounding the slab ( $S_3 \equiv S_1$ ), the four channel scattering matrix  $\mathbf{S}$  built up from the conservation of the energy flow vector perpendicularly to the interfaces (Franklin *et al.* (2001)) is

$$\mathbf{S} = \begin{bmatrix} r_1^{LL} & t_1^{LL} & \beta r_1^{LT} & \beta t_1^{LT} \\ t_1^{LL} & r_1^{LL} & -\beta t_1^{LT} & -\beta r_1^{LT} \\ \beta t_1^{LT} & -\beta t_1^{LT} & -r_1^{TT} & -t_1^{TT} \\ \beta t_1^{LT} & -\beta r_1^{LT} & -t_1^{TT} & -r_1^{TT} \end{bmatrix} \quad (3)$$

with the normalization coefficient  $\beta = (k_{zT,1}/k_{zL,1})^{1/2}$ .  $\mathbf{S}$  is a symmetric and unitary matrix ( $\mathbf{S}^\dagger \mathbf{S} = \mathbf{S} \mathbf{S}^\dagger = \mathbf{I}$ , where  $^\dagger$  is the adjoint operator). In the following, the study will be limited to the case of light fluids ( $c_F < c_{T,1} < c_{L,1}$ ), and the different graphics will be plotted for a water slab  $F_2$  (thickness  $d = 5$  mm, density  $\rho_F = 1000$  kg.m<sup>-3</sup>, phase velocity  $c_F = 1470$  m.s<sup>-1</sup>) in aluminum solid  $S_1$  (density  $\rho_{S,1} = 2790$  kg.m<sup>-3</sup>, longitudinal and transversal phase velocities  $c_{L,1} = 6380$  m.s<sup>-1</sup> and  $c_{T,1} = 3100$  m.s<sup>-1</sup>).

## 2 Analysis of the $\mathbf{S}$ matrix : resonant and background scattering.

The  $\mathbf{S}$  matrix formalism offers a powerful tool to break apart scattering mechanisms into simple and understandable contributions. As the analytical determination of the  $\mathbf{S}$  eigenvalues from the characteristic equation  $\det(\mathbf{S} - \lambda \mathbf{I}) = 0$  is difficult, a way to obtain these quantities consists in the study of the  $(2 \times 2)$ -subminors of the determinant  $\det(\mathbf{T})$  of the transition matrix  $\mathbf{T} = (\mathbf{S} - \mathbf{I})/(2j)$ . This provides the remarkable identities written as follows :

$$(r_1^{LL} - 1) / \beta r_1^{LT} = -t_1^{LL} / \beta t_1^{LT} = -\beta r_1^{LT} / (r_1^{TT} + 1) = -\beta t_1^{LT} / t_1^{TT}. \quad (4)$$

The use of the previous relations enables to factorize easily the characteristic polynomial  $\det(\mathbf{S} - \lambda \mathbf{I})$ . Finally, the four unitary eigenvalues of  $\mathbf{S}$  are  $\lambda = \{S_S, S_A, 1, 1\}$  where

$$S_{S/A} = r_1^{LL} - r_1^{TT} \pm (t_1^{LL} + t_1^{TT}) = -(C_{S/A,1} \pm j\tau_1) / (C_{S/A,1} \mp j\tau_1), \quad (5)$$

The open eigenchannels -associated with the eigenvalues  $S_S$  and  $S_A$ - correspond respectively to symmetric-longitudinal and antisymmetric-longitudinal polarizations. The eigenchannels associated with the double eigenvalue equal to 1 are closed and should correspond respectively to symmetric-transversal and antisymmetric-transversal polarizations if these channels were open (*i.e.* in the case of a solid slab for example).

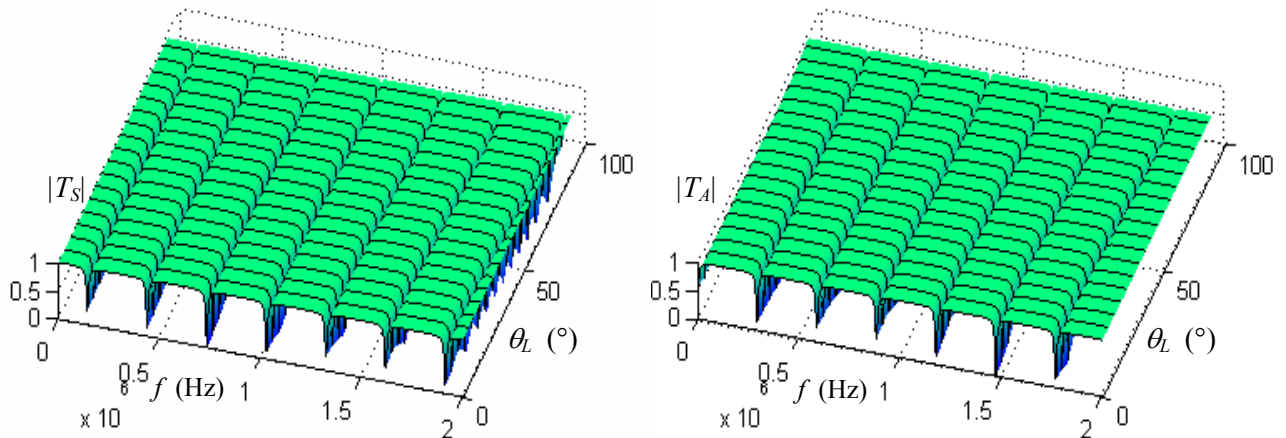


FIG. 2 – Plot in the  $(f, \theta_L)$ -plane of the non null eigenvalue moduli of the transition matrix (left :  $|T_S|$ ; right :  $|T_A|$ ).

As a consequence, only two eigenvalues of the transition eigenmatrix  $\mathbf{T}_{\text{eig}} = (\mathbf{S}_{\text{eig}} - \mathbf{I})/(2j)$  defined from the scattering eigenmatrix  $\mathbf{S}_{\text{eig}} = \text{diag}\{S_S, S_A, 1, 1\}$  are non null and denoted as  $T_{S/A} = (S_{S/A} - 1)/(2j)$ . The plots of their moduli in the (frequency, longitudinal incidence angle)-plane ( $f, \theta_L$ ) are given in FIG.2. They both exhibit antiresonances (in fact, resonances in counterphase with a constant transition amplitude component). Compared to other resonant scattering problems (Rembert *et al.* (2004)), this behavior can be easily explained by separating the whole scattering amplitudes as a combination of non resonant (or background) scattering terms and purely resonant scattering contributions. Mathematically speaking, the shape of the transition amplitudes is mainly due to the minus (-) sign that occurs in front of the non unimodular eigenvalues of  $\mathbf{S}$  in Eq. (5). Indeed, when plotting the transition amplitudes  $T_{S/A}^{(*)} = (-S_{S/A} - 1)/(2j)$  instead of  $T_{S/A}$ , one obtains a pure Breit-Wigner resonance spectrum (see FIG. 3). Indeed, at a given incidence angle  $\theta_L$ , a first order expansion of  $T_{S/A}^{(*)}$  shows that each resonance frequency is close to a root of  $C_{S/A,1} = 0$  and each resonance half-width is nearly equal to  $\pm \tau_1 / (\partial C_{S/A,1} / \partial x)$ . As a consequence, the scattering eigenmatrices  $\mathbf{S}_{\text{eig}}^{(b)} = \text{diag}\{-1, -1, 1, 1\}$  and  $\mathbf{S}_{\text{eig}}^{(*)} = \text{diag}\{-S_S, -S_A, 1, 1\}$  are defined so that

$$\mathbf{S}_{\text{eig}} = \mathbf{S}_{\text{eig}}^{(b)} \mathbf{S}_{\text{eig}}^{(*)} \quad (7)$$

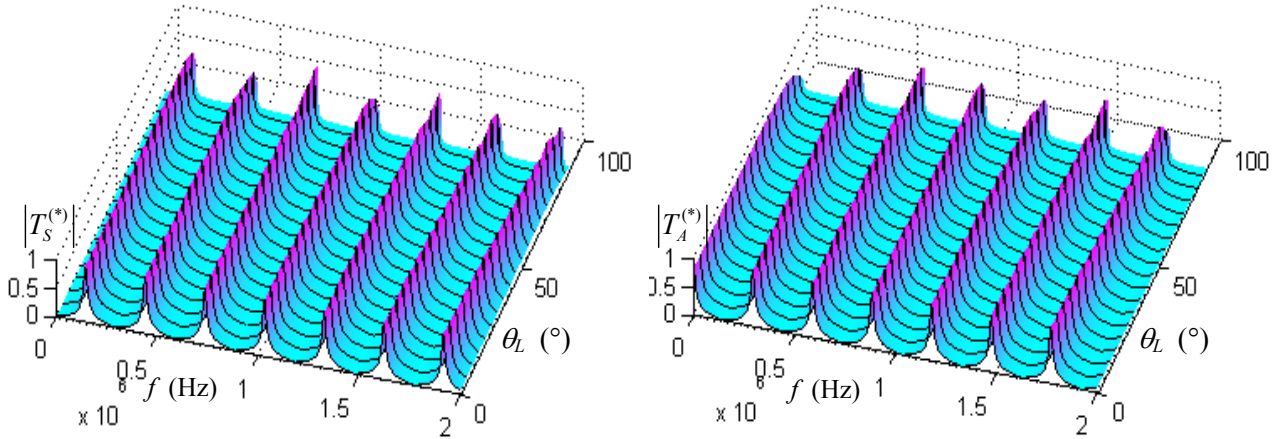
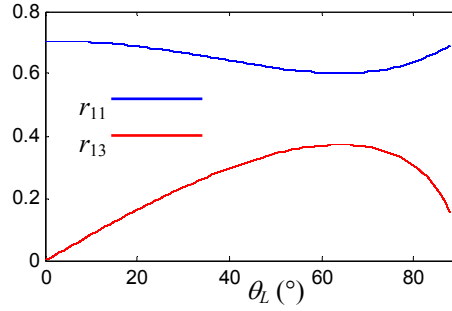


FIG. 3 – Plot in the ( $f, \theta_L$ )-plane of the resonant eigentransition amplitudes (left :  $|T_S^{(*)}|$  ; right :  $|T_A^{(*)}|$ ).

In order to connect these eigenmatrices with the original scattering matrix  $\mathbf{S}$ , the calculation of the eigenvectors is straightforwardly processed. Once normalized, the real rotation matrix  $\mathbf{R}$  involved in the change of basis relation,  $\mathbf{S} = \mathbf{R} \mathbf{S}_{\text{eig}} \mathbf{R}^\dagger$ , is

$$\mathbf{R} = [r_{ij}] = \frac{1}{\sqrt{2}\sqrt{1+\gamma^2}} \begin{bmatrix} 1 & 1 & \gamma & \gamma \\ -1 & 1 & \gamma & -\gamma \\ -\gamma & -\gamma & 1 & 1 \\ -\gamma & \gamma & -1 & 1 \end{bmatrix}, \quad (8)$$

where  $\gamma = \sqrt{(R_1^+ + R_1^-)/(R_1^+ - R_1^-)}$ . As they do not depend on the frequency, the components  $r_{11}$  and  $r_{13}$  of  $\mathbf{R}$  are plotted versus the longitudinal incidence angle  $\theta_L$  in FIG. 4.

FIG. 4 – Plot of the  $r_{11}$  and  $r_{13}$  components of  $\mathbf{R}$  versus  $\theta_L$ 

Introducing the change of basis relations  $\mathbf{S}^{(*)} = \mathbf{R}\mathbf{S}_{\text{eig}}^{(*)}\mathbf{R}^t$  and  $\mathbf{S}^{(b)} = \mathbf{R}\mathbf{S}_{\text{eig}}^{(b)}\mathbf{R}^t$ , the scattering matrix  $\mathbf{S}$  is factorized as the product  $\mathbf{S} = \mathbf{S}^{(b)}\mathbf{S}^{(*)}$ .  $\mathbf{S}^{(*)}$  describes the pure resonant scattering of the fluid slab, and  $\mathbf{S}^{(b)}$  the non resonant scattering of the slab. More precisely, it is demonstrated that  $\mathbf{S}^{(b)}$  is nothing but the  $\mathbf{S}$  matrix written in the particular case  $\rho_F = 0$ , *i.e.* the scattering by a vacuumed slab. In that case, the scattering coefficients related to the transmission terms vanish and the components of  $\mathbf{S}^{(b)}$  only depend on the rotation matrix  $\mathbf{R}$ .

### 3 Wigner-Smith matrix

The time-delay or Wigner-Smith matrix  $\mathbf{Q}_x$  is defined from the scattering matrix as

$$\mathbf{Q}_x = -j(\partial_x \mathbf{S})\mathbf{S}^\dagger. \quad (9)$$

Recalling that  $\mathbf{S}^{-1} = \mathbf{S}^\dagger$ ,  $\mathbf{Q}_x$  is the generalized logarithmic derivative of  $\mathbf{S}$  with respect to a parameter  $x$  involved in the expression of the scattering matrix elements. This matrix is self-adjoint ( $\mathbf{Q}_x = \mathbf{Q}_x^\dagger$ ) and its eigenvalues are pure phase partial derivatives with respect to  $x$ , connected with the eigenphase derivatives of  $\mathbf{S}$  (Franklin *et al.* (2006)).  $\mathbf{Q}_x$  is the multichannel generalization of the Phase Gradient Method used to investigate the resonant phase of scattering coefficients (Lenoir, *et al.* 2003). Considering the particular set of parameters  $x_{i=1..4} = (f, c_F, c_{L,1}, c_{T,1})$ , it is shown, as in the cases of one channel and two channel scattering (Lenoir, *et al.* 2003, Franklin *et al.* 2006), that the remarkable equation

$$\sum_{i=1}^4 x_i \mathbf{Q}_{x_i} = 0, \quad (10)$$

is still verified. When written at a resonance frequency of the scatterer, this relation represents a reactive power balance. Another interest of the  $\mathbf{Q}_x$  formalism lies obviously in the linearization of each possible factorization of  $\mathbf{S}$ . Inserting the change of basis relation  $\mathbf{S} = \mathbf{R}\mathbf{S}_{\text{eig}}\mathbf{R}^\dagger$  in definition (9) gives

$$\mathbf{Q}_x = \mathbf{Q}_x^{(*)} + \mathbf{Q}_x^{(p)}. \quad (11)$$

In the previous relation,  $\mathbf{Q}_x^{(*)} = -j\mathbf{R}(\partial_x \mathbf{S}_{\text{eig}}^{(*)})\mathbf{S}_{\text{eig}}^{(*)\dagger}\mathbf{R}^t$  is the purely resonant part of  $\mathbf{Q}_x$  related to  $\mathbf{S}^{(*)}$ : its eigenmatrix is  $(\partial_x \mathbf{S}_{\text{eig}}^{(*)})\mathbf{S}_{\text{eig}}^{(*)\dagger} = \text{diag}\{-2\partial_x \delta_S^{(*)}, -2\partial_x \delta_A^{(*)}, 0, 0\}$ , where  $-\delta_{S/A}^{(*)}$  are the half resonant eigenphases of  $\mathbf{S}$  (*i.e.*  $S_{S/A} = -\exp(-j2\delta_{S/A}^{(*)})$ ), the trace of  $\mathbf{Q}_x^{(*)}$  is a pure Breit-Wigner resonance spectrum (each resonance peak height are twice the inverse of their width).  $\mathbf{Q}_x^{(p)}$  is

the potential contribution of  $\mathbf{Q}_x$  but slightly different from the background scattering due to  $\mathbf{S}^{(b)}$ . Indeed, its eigenmatrix  $\mathbf{Q}_{x,eig}^{(p)}$  depends on the half resonant eigenphases :

$$\mathbf{Q}_{x,eig}^{(p)} = \text{diag} \{ \cos(\delta_S^{(*)}), \cos(\delta_A^{(*)}), -\cos(\delta_A^{(*)}), -\cos(\delta_S^{(*)}) \} \times \partial_x \gamma / (1 + \gamma^2). \quad (12)$$

$\mathbf{Q}_x^{(p)}$  is a null trace matrix, proving that  $\text{tr}(\mathbf{Q}_x) = \text{tr}(\mathbf{Q}_x^{(*)})$  contains the whole resonant information about the scatterer. In the particular case  $x = f$ ,  $\mathbf{Q}_x^{(p)}$  is null ( $\gamma$  is independent of  $f$ ) and then,  $\mathbf{Q}_f = \mathbf{Q}_f^{(*)}$ . In Fig. 5, the first symmetric eigenvalues of  $\mathbf{Q}_{c_F}^{(*)}$  and  $\mathbf{Q}_{c_F}^{(p)}$  are plotted in the  $(f, \theta_L)$ -plane : their respective amplitudes clearly indicate that the role of the potential scattering is negligible compared to the resonant scattering in  $\mathbf{Q}_{c_F}$ .

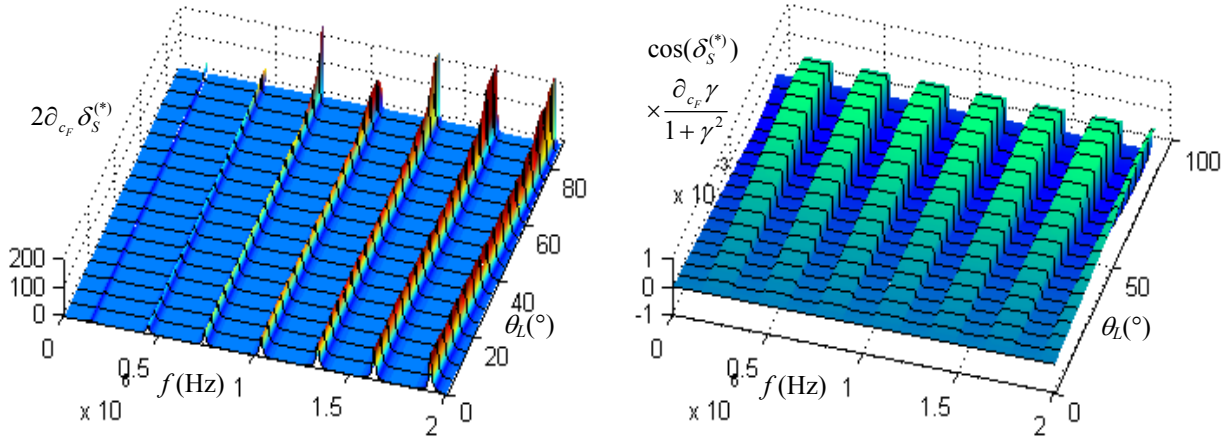


FIG. 5 – Plots in the  $(f, \theta_L)$ -plane of the symmetric eigenvalues of  $\mathbf{Q}_{c_F}^{(*)}$  (left), and  $\mathbf{Q}_{c_F}^{(p)}$  (right).

## 5 Conclusive remarks

The Wigner-Smith matrix  $\mathbf{Q}$  formalism is a natural filtering tool to isolate resonant contributions in a many scattering channel situation. This ability concerns, not only the frequency variable, but all the indepent input parameters of the problem. The  $\mathbf{S}$  matrix formalism is used as a “*preprocessing engine*” in order to exploit fully the  $\mathbf{Q}$  matrix properties.

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